

A SUCCESSIVE IMPACT OF TEMPERATURE AND IRRADIANCE ON LIFETIME OF PV INVERTER

M Sivanageswara rao ¹, V Suresh Kumar ², G Gopayya ³

¹ Associate Professor, ² Associate Professor, ³ Assistant professor

Department of Electrical and Electronics Engineering
Priyadarshini Institute of Technology & Science, Tenali, Guntur

Abstract: - Age of PV inverters will be affected from the foundation areas related to different sun situated irradiant and encompassing high temperature profiles (also implied toward being essential). All things considered, the foundation site in like manner impacts the degradation speed of the PV sheets, and thusly long stretch essentialness creation and constancy. Prior workmanship lifetime assessment in PV INV's haven't till investigated any impact of the PV load up defilements. In the paper as needs be evaluates the age of PV INV worried about board degradation expenses and assignment profiles. Evaluations has finished at PV systems presented in Himachal Pradesh and Tamilnadu. Results reveal at the PV board degradation pace impressively influences the PV INV period, especially in the warm air (e.g., Tamilnadu), There the board defiles in faster rate. In light of everything, the PV INV period gauge will be veered off at 54 %, in the event that the impact of PV board defilements.

Index Terms—PV INV, generation, reliability, mission profile, degradation,

Photovoltaic (PV) advancement might perhaps transform into a critical essentialness source in the near future, then, at that point, has experienced a greater improvement rank through the most as of late in once in decade [1]. As more PV systems has been presented then connected with an organization, with the immovable quality then age are expanding progressively massively thought [2]-[4]. The continuous development, the period of PV loads up ordinarily legitimized in 20-25 years, while the PV INV lifetime by and large limited to bring down level in 15 years [5]. Consequently, the PV INV will be represented as the most fundamental parts which cause frustrations at the entire PV systems [6], [7]. At network related PV structures, the cost connected with the PV INV disillusionment can be around 59 % in full scale system cost [8].

Age of lattice related PV INV will be essentially affected with the functioning conditions, that would impact any warm stacking in the power devices [9]-[11]. It tends to be a result of different control strategies at the PV [12]-[15], yet moreover the foundation areas Studies have uncovered that the foundation region significantly

1. INTRODUCTION

influences the enduring quality and lifetime of PV INVs. Conversely, some foundation regions arranged in the northern piece of the world regularly have a for the most part low ordinary daylight based irradiant stage all through stormy climate and summer situated irradiant blueprint could vary amazingly over time. Tantamount tendency is also inferred in the encompassing degree of temperature framework of the foundation point.

In any case, Earlier thing of beauty didn't consider the impact of PV load up corruptions in the lifetime evaluation. Accordingly, it is regularly expected in the PV power creation then the warm stacking of the PV INV is rehashed annually for specific establishment destinations. Hence, the Life Consumption (LC) of the PV INV, demonstrating amount of the life of INV is expended, will typically decided for example an yearly crucial.

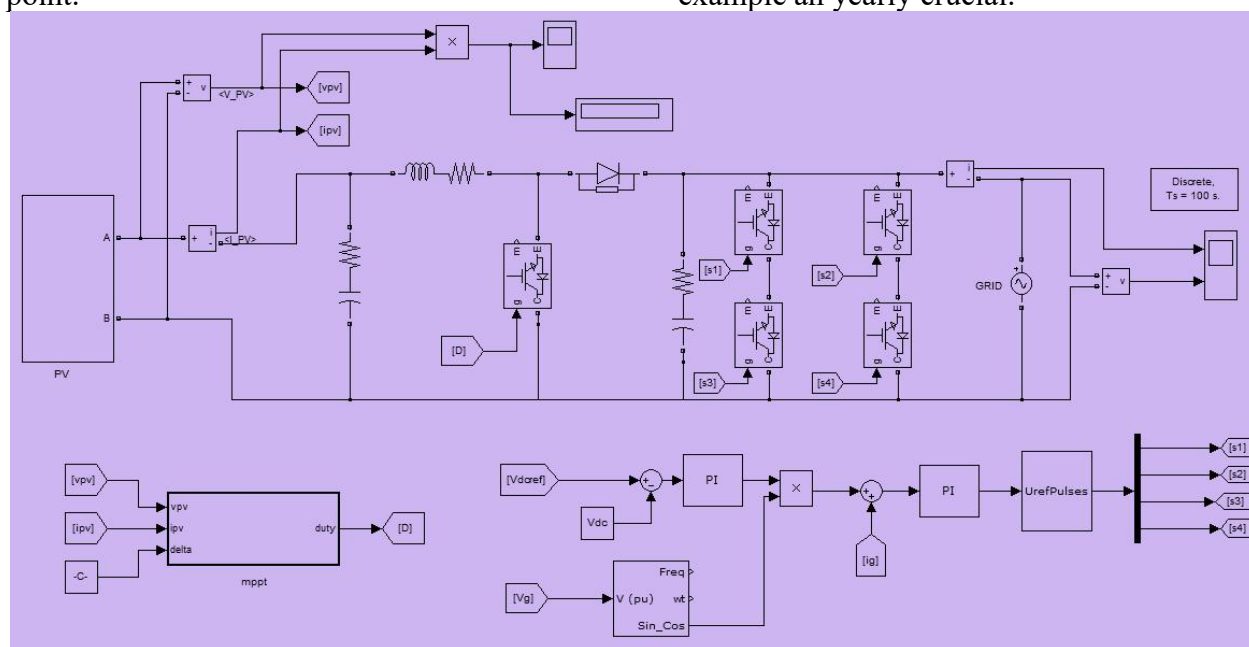


Fig. 1. System configuration and control structure of a two-stage single-phase grid-connected PV system (PI - Proportional Integral, PLL - Phase Locked Loop, PWM - Pulse Width Modulation).

As per from above conversations, clearly the PV board corruption directly affects the drawn out warm stacking of the PV INV, and hence its era forecast. As to speak to a more sensible working circumstances and enhance the era assessment precision of the PV INV, the debasement paces of the PV boards at

various establishment areas must be considered.

TABLE I
PARAMETERS OF THE BP 365 SOLAR
PV PANEL AT THE STC.

Panel rated power	$P_{mpp} = 65$ W
Voltage at the maximum power point	$V_{mpp} =$ 17.6 V
Current at the maximum power point	$I_{mpp} = 3.69$ A
Open-circuit voltage	$V_{OC} = 21.7$ V
Short-circuit current	$I_{SC} = 3.99$ A

TABLE II
PARAMETERS OF THE TWO-STAGE
SINGLE-PHASE PV SYSTEM (FIG.1)

PV inverter rated power	6 kW
Boost converter inductor	$L = 1.8$ mH
PV-side capacitor	$C_{pv} = 1000$ F
DC-link capacitor	$C_{dc} = 1100$ F
LCL-filter	$L_{inv} = 4.8$ mH, $L_g =$ 2 mH, $C_f = 4.3$ F
Switching frequency	Boost converter: $f_b =$ 16 kHz, Full-Bridge inverter: $f_{inv} = 8$ kHz
DC-link voltage	$v_{dc} = 450$ V
Grid nominal voltage (RMS)	$V_g = 230$ V
Grid nominal frequency	$\omega = 2\pi \cdot 50$ rad/s

The remainder of the paper is sorted out as given: the depiction of the contextual analysis can be given in Section II. At that

point, the strategic based era assessment is introduced in Section III. The era assessment and the dependability appraisal of the contextual analysis are completed in Sections IV and V, separately. At last, closing comments are given in Section VI.

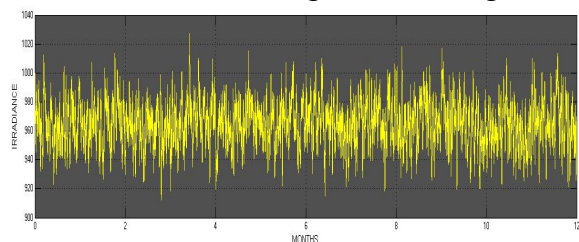
II.DESCRPTION OF THE CASE STUDY

A. System Description

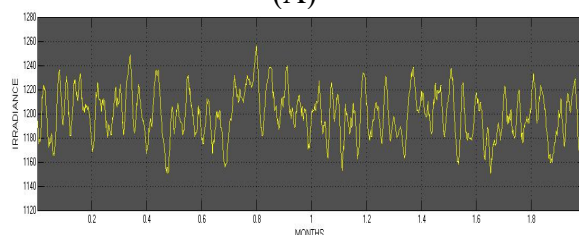
The BP365 PV board is utilized in this investigation, where the board trademark at the Standard Test Condition (STC) is given in Table I. For this situation, a PV string comprises of 15 PV boards, and 6 PV strings are associated in equal so as to accomplish the appraised power around 6 kW. At that point, a two-phase PV framework comprising of a lift dc-dc converter and a full extension dc-air conditioning INV (PV INV) is utilized as the interface between the PV boards and the air conditioner lattice. The framework arrangement is appeared in Fig. 1, and its boundaries are given in Table II.

This two-phase arrangement is broadly utilized in private PV frameworks where the Maximum Power Point Tracking activity is actualized in the lift converter. At that point, the PV conveys the extricated capacity to the air conditioner framework by managing the dc-connect voltage v_{dc} to be consistent. So as to do as such, the current regulator is acting to manage the matrix current i_g as per a reference given by the dc-

interface voltage regulator.



(A)



(B)

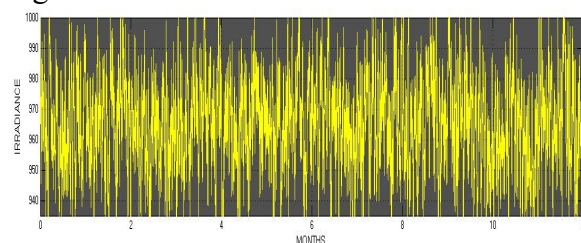
Fig. 2. Yearly mission profiles from the installation site in Himachal Pradesh with a sampling rate of 5 mins per sample: (a) solar irradiance and (b) ambient temperature

B. Mission Profile of the PV Systems

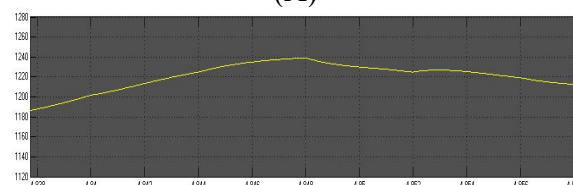
So as to assess the lifetime of the PV INV under genuine working conditions, a strategic, which is a portrayal of the working state of the framework, is required [11]. On account of PV applications, the sunlight based irradiance and encompassing temperature are considered as crucial, since the PV power creation is unequivocally subject to the two boundaries.

In this paper, two crucial recorded in Himachal Pradesh and Tamilnadu appeared in Figs. 2 and 3 are utilized. It very well may be seen from the crucial that the normal sun powered irradiance level in Tamilnadu is continually high consistently, while it is generally low in Himachal Pradesh through November to February.

The mission profiles in Figs. 2 and 3 speak to two distinct situations where the PV frameworks are introduced in: 1) a normal low sunlight based irradiance and surrounding temperature area a normal high sun based irradiance and encompassing temperature area It can be normal that the PV power creation in Tamilnadu will be higher than in Himachal Pradesh.



(A)



(B)

Fig.3. Yearly mission outlines from the connection site in Tamilnadu with a sampling rate of 5 mins per sample: (a) solar irradiance and (b) ambient Temp.

B. Squalor Rate of the PV Panels

As referenced already, the long haul PV power creation isn't just controlled by the mission profile of the PV framework, yet additionally on the corruption pace of the PV boards. Studies have demonstrated that the PV board corruption rate differs significantly as indicated by the establishment area. These enormous varieties in the debasement rate are fundamentally affected by various atmosphere states of the establishment

locales An investigation of the gathered genuine field information has been done.

Likewise, the board debasement attributes ought to likewise be considered while considering the PV board corruption impacts.

As indicated by the investigation, the corruption normal for the PV board can be fluctuated by the PV board disappointment mode For example, an exemplify staining, which is one of the most regularly revealed disappointment modes in PV boards, as a rule prompts a straight debasement of PV boards where the PV power creation diminishes directly after some time. Then again, a non-straight debasement conduct can be seen in some PV boards with weld bond exhaustion and bind bond disappointment.

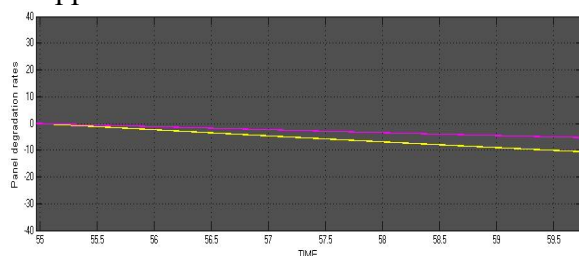


Fig. 4. Degradation profiles of the PV panels installed in Himachal Pradesh and Tamilnadu with the degradation rate of 0.15 %/year and 1 %/year, respectively.

On the other hand, the PV board debasement rate can likewise be resolved from genuine field estimations, as it has been finished. All things considered, a direct debasement trademark is typically accepted, where the corruption profile is gotten from the genuine field estimated. Indeed, this is really appropriate for some pragmatic cases,

where the PV board isn't regularly portrayed during activity. For example, it has been accounted for that the estimation of PV board yield power at the STC is typically done once during the whole life expectancy, bringing about a predetermined number of information focuses [26].

All things considered, it bodes well to apply the direct corruption model for the PV boards. Nonetheless, it is worth to specify that the exactness of the corruption model is undermined with this methodology because of the rearranged straight model. Some down to earth perspectives, for example, non uniform corruption rate over the whole PV plant or halfway concealing impact can't be considered. By and by, it offers a basic yet down to earth answer for a drawn out reenactment without requiring a huge arrangement of estimation information or nitty gritty model of the PV board.

Considering the above conversations, a straight debasement model dependent on the estimation information will be considered in this paper. In this investigation, the debasement pace of 0.15 %/year in Himachal Pradesh and 1 %/year in Tamilnadu are utilized, as per the field estimations. The yearly debasement profile of the PV boards at these areas is shown in Fig. 4. By the by, it ought to be referenced that the strategic based lifetime assessment introduced in this paper can likewise be commonly applied to any discretionary corruption trademark This will be additionally tended to in the crucial

interpretation measure in the accompanying segment.

III. MISSION PROFILE-BASED LIFETIME ESTIMATION

A system is required to assess the lifetime of the PV INV below convinced strategic. This is on the grounds that the lifetime model of the basic segments in the PV INV normally identifies with the temperature varieties [4]. Subsequently, the mission profile ought to be first converted into the warm stacking of the PV INV.

Warm stacking of the PV INV. Indeed, the intersection temperature varieties are identified with the force misfortunes P_{loss} disseminated in the influence gadget and the cooling framework. In this manner, there are halfway strides between these interpretations, which identifies with the force created at each stage.

To start with, the accessible PV intensity of the PV clusters P_{mpp} is resolved from the sun oriented irradiance and surrounding

temperature profiles by utilizing the board trademark model. Thusly, the time-differing accessible PV power profile can be gotten. This is as opposed to the past work, where the accessible PV power P_{mpp} is legitimately deciphered as the genuine PV yield power from the PV clusters P_{pv} during the whole activity.

Thereafter, the force misfortunes P_{loss} dispersed in the influence gadgets can be determined by taking the MPPT activity productivity (99 %) and the PV INV proficiency into account. When the force misfortunes P_{loss} are determined, the gadget intersection temperature profile T_j can be acquired from the warm model of the influence gadget. This warm model likewise thinks about the encompassing temperature of the PV INV, as it influences the influence gadget intersection temperature varieties. Notably, this cycle is actualized by utilizing a Lookup Table (LUT) created from the influence gadget electrical trademark.

A. Cycle Counting using Rain flow Analysis

The intersection temperature variety acquired from the past advance is a sporadic profile, as per the mission profile. So as to apply such an intersection temperature outline to the lifetime classical, an including calculation, for example, a downpour stream examination is required [10].

Lifetime Model of the PV INVs (Power devices)

The lifetime assessment of the whole PV INV requires top to bottom information

regarding numerous matters, since the segments in the PV framework can have cross impacts of the dependability among one another. So as to improve the investigation, the lifetime of the force gadget is just viewed as here.

TABLE III
PARAMETERS OF THE LIFETIME
MODEL OF AN IGBT MODULE [43]

A	3.4368×10^4	
α	-4.923	$64 \text{ K} \leq T_j \leq 113 \text{ K}$
B_1	-9.012×10^{-3}	
B_0	1.942	$0:19 \leq ar \leq 0:42$
C	1.434	
γ	-1.208	$0:07 \text{ s} \leq ton \leq 63 \text{ s}$
f_d	0.6204	
E_a	0.06606eV	$32:5 \leq C \leq T_j \leq 122$ $\leq C$
k_b	$8.6173324 \times 10^{-}$	

The LC is then calculated by using the Miner's rule [10] as

$$LC = \sum_i^0 \left(\times \frac{n_i}{N_{fi}} \right) \dots \dots (1)$$

The LC can be utilized to show how much the life of the force gadget is expended during activity. For example, if the quantity of cycles n_i is tallied from a yearly strategic, the LC determined in (1) will speak to a yearly LC of the force gadget. The lifetime of the force gadget is then decided when the LC collects to solidarity, which is the point at which the gadget arrives at its finish of life.

IV. LIFETIME EVALUATION (CASE STUDY)

In this segment, the lifetime assessment examined in Section III is applied to the contextual analysis. The intersection temperature varieties and the LC of the force gadget are analyzed.

A. Junction Temperature Variations

The intersection temperature variety is a result of the force gadget stacking. In this respect, the effect of PV board debasements can be seen in the intersection temperature varieties in the PV INVs. Because of the higher normal irradiance level in Tamilnadu, the mean intersection temperature T_{jm} of the PV INV in Tamilnadu is all in all higher

than in Himachal Pradesh. It tends to be seen from Fig. 6 that the mean intersection temperature in Tamilnadu is around 3°C lower contrasted with the primary year, while the decrease in the mean intersection temperature is extremely little in Himachal Pradesh.

B. Lifetime Evaluation

The yearly LC of the force gadget is determined for an activity of 20 years so as to watch the effect of the board debasement in the long haul LC.

For this situation, bend fitting is additionally applied so as to get the aggregate LC following an activity of 20 years. The force gadget is considered to bomb when the combined LC arrives at solidarity, and the lifetime would then be able to be acquired. The total LC without considering the debasement rate is additionally appeared for examination, where the assessed lifetime goes amiss significantly in the two cases.

V. CONCLUSION

The effect of the PV board debasement on the period assessment of PV INVs has been introduced in this paper. The assessment depends on the task profiles with hot atmosphere (i.e., Tamilnadu) and cold atmosphere (i.e., Himachal Pradesh) situations, where the corruption pace of the PV board at the 2 areas has additionally been considered.

The examination uncovers that the warm stacking and the existence utilization of the PV INVs decline significantly during activity, particularly in the hot atmosphere

where the PV board debases quick. In this condition, the assessed lifetime can be veered off by 54 % if the board debasement isn't considered. As needs be, the PV board debasement affects the lifetime of PV INV, and accordingly must be considered in the lifetime assessment and furthermore in the structure stage.

REFERENCES

- [1] REN21, "Renewable 2016: Global Status Report (GRS)," 2016. [Online]. Available: <http://www.ren21.net/>.
- [2] G. Petrone, G. Spagnuolo, R. Teodorescu, M. Veerachary, and M. Vitelli, "Reliability issues in photovoltaic power processing systems," *IEEE Trans. Ind. Electron.*, vol. 55, no. 7, pp. 2569–2580, Jul. 2008.
- [3] Y. Song and B. Wang, "Survey on reliability of power electronic systems," *IEEE Trans. Power Electron.*, vol. 28, no. 1, pp. 591–604, Jan. 2013.
- [4] H. S.-H. Chung, H. Wang, F. Blaabjerg, and M. Pecht, *Reliability of Power Electronic Converter Systems*. IET, 2015.
- [5] National Renewable Energy Laboratory, "On the path to sunshot: The role of advancements in solar photovoltaic efficiency, reliability, and costs," Tech. Rep. No. NREL/TP-6A20-65872, 2016.
- [6] A. Golnas, "PV system reliability: An operator's perspective," *IEEE J. of Photovolt.*, vol. 3, no. 1, pp. 416–421, Jan. 2013.
- [7] C. A. F. Fernandes, J. P. N. Torres, M. Morgado, and J. A. P. Morgado, "Aging of solar PV plants and mitigation of their consequences," in *Proc. of PEMC*, pp. 1240–1247, Sep. 2016.
- [8] L. M. Moore and H. N. Post, "Five years of operating experience at a large, utility-scale photovoltaic generating plant," *Progress Photovoltaics: Res. Appl.*, vol. 16, no. 3, pp. 249–259, 2008.
- [9] H. Wang, M. Liserre, and F. Blaabjerg, "Toward reliable power electronics: Challenges, design tools, and opportunities," *IEEE Ind. Electron. Mag.*, vol. 7, no. 2, pp. 17–26, Jun. 2013.
- [10] H. Huang and P. A. Mawby, "A lifetime estimation technique for voltage source INVs," *IEEE Trans. Power Electron.*, vol. 28, no. 8, pp. 4113–4119, Aug. 2013.
- [11] M. Musallam, C. Yin, C. Bailey, and M. Johnson, "Mission profilebased reliability design and real-time life consumption estimation in power electronics," *IEEE Trans. Power Electron.*, vol. 30, no. 5, pp. 2601–2613, May 2015.
- [12] M. Andresen, G. Buticchi, and M. Liserre, "Thermal stress analysis and MPPT optimization of photovoltaic systems," *IEEE Trans. Ind. Electron.*, vol. 63, no. 8, pp. 4889–4898, Aug. 2016.
- [13] A. Anurag, Y. Yang, and F. Blaabjerg, "Thermal performance and reliability analysis of single-phase PV INVs with reactive power injection outside feed-in operating hours," *IEEE Trans. Emerg. Sel. Topics Power Electron.* vol. 3, no. 4, pp. 870–880, Dec. 2015.
- [14] Y. Yang, H. Wang, and F. Blaabjerg, "Improved reliability of single-phase PV INVs by limiting the maximum feed-in

power,” in Proc. of ECCE, pp. 128–135, Sep. 2014.

[15] Y. Yang, E. Koutroulis, A. Sangwongwanich, and F. Blaabjerg, “Minimizing the levelized cost of energy in

single-phase photovoltaic systems with an absolute active power control,” IEEE Ind. Appl. Mag., vol. 23, no. 5, pp. 1–10, Sep./Oct. 2017.